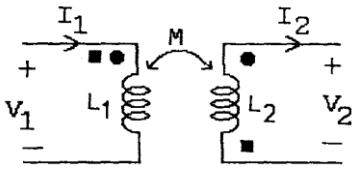


**Mutual Inductance and Linear Transformers**



Round dots:

$$\begin{aligned}\vec{V}_1 &= j\omega L_1 \vec{I}_1 - j\omega M \vec{I}_2 \\ \vec{V}_2 &= +j\omega M \vec{I}_1 - j\omega L_2 \vec{I}_2\end{aligned}$$

Square dots:

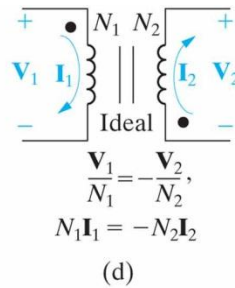
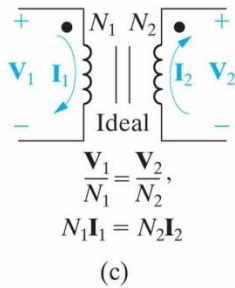
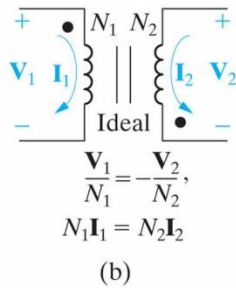
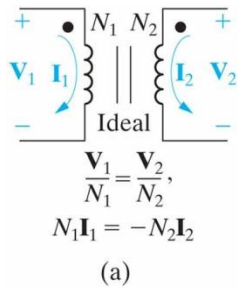
$$\begin{aligned}\vec{V}_1 &= j\omega L_1 \vec{I}_1 + j\omega M \vec{I}_2 \\ \vec{V}_2 &= -j\omega M \vec{I}_1 - j\omega L_2 \vec{I}_2\end{aligned}$$

Reflected impedance  $Z_r = \frac{\omega^2 M^2}{|Z_{22}|^2} [(R_2 + R_L) - j(\omega L_2 + X_L)]$  where  $Z_{22} = R_2 + R_L + j(\omega L_2 + X_L)$

$$M = k\sqrt{L_1 L_2}$$

$$w(t) = \frac{L_1 i_1^2}{2} + \frac{L_2 i_2^2}{2} \pm i_1 i_2 M$$

**Ideal Transformers**



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The impedance seen by the source  $Z_{in} = \frac{V_1}{I_1} = \frac{1}{a^2} \frac{V_2}{I_2} = \frac{1}{a^2} Z_L$  where  $a = \frac{N_2}{N_1}$

AC Information	Quantity	Symbol	Unit	Formulas
$v = V_m \cos(\omega t + \phi) \quad f = \frac{1}{T} = \frac{\omega}{2\pi}$ $V = ZI \quad \vec{V}_{eff} = Z \vec{I}_{eff}$	Complex power	S	VA	$S = \vec{V} \vec{I}^*$ $= V_{rms} I_{rms} \angle \theta$ $= P + jQ = I_{rms}^2 Z$
Rectangular to Polar conversion $V = A + jB = \sqrt{A^2 + B^2} \angle \left( \tan^{-1} \frac{B}{A} \right)^\circ$	Apparent power	S	VA	$ S  = V_{rms} I_{rms}$ $= \sqrt{P^2 + Q^2}$
Polar to Rectangular conversion $V = V_m \angle \phi^\circ = V_m \cos \phi + j V_m \sin \phi$ (Note that $V_m$ is a magnitude and should be positive, thus angle needs to reflect the change)	Average power	P	W	$P = \text{Re}\{S\}$ $= V_{rms} I_{rms} \cos \theta$ $= I_{rms}^2 \text{Re}\{Z\}$
Complex Number Identities $j^2 = -1 \quad \text{and} \quad \frac{1}{j} = -j$	Reactive power	Q	var	$Q = \text{Im}\{S\}$ $= V_{rms} I_{rms} \sin \theta$ $= I_{rms}^2 \text{Im}\{Z\}$
<u>Lagging power factor</u> : implies that the current lags the voltage – hence <i>inductive load</i>	Instantaneous power	p(t)	W	$p(t) = P + P \cos 2\omega t + Q \sin 2\omega t$
<u>Leading power factor</u> : implies that the current leads the voltage – hence <i>capacitive load</i>	Power factor angle	$\theta$	deg	$\theta = \angle S = \angle Z$ $= \angle \vec{V} - \angle \vec{I}$
	Power factor	pf		Lagging if $\theta > 0$ & $Q > 0$ ; leading if $\theta < 0$ & $Q < 0$ . $pf = \frac{P}{ S } = \cos \theta$

**BALANCED THREE-PHASE SYSTEMS:**

Balanced source: equal magnitudes; phase angle separated by 120 deg

Balanced load or line: equal phase impedances

Balanced system = balanced source + balanced line + balanced load

Phase powers are equal:  $S_A = S_B = S_C$

Total 3Φ power = 3 times the per-phase power; e.g.,  $S_{3\Phi} = 3 * S_A$

Y-Connection assuming abc-sequence:

$$\vec{V}_{ab} = (\sqrt{3}\angle 30^\circ)\vec{V}_{an} \quad \text{or} \quad V_L = \sqrt{3}V_\phi \quad [\text{magnitude only}] \quad \text{Same for load end}$$

$$\text{Line current} = \text{phase current: } \vec{I}_{aA} = \vec{I}_{AN} \quad \text{or} \quad I_L = I_\phi \quad [\text{magnitude only}]$$

Δ-Connection assuming abc-sequence:

$$\Delta\text{-to-Y Transformation: } Z_Y = \frac{1}{3}Z_\Delta$$

$$\text{Line voltage} = \text{phase voltage} = \vec{V}_{AB}$$

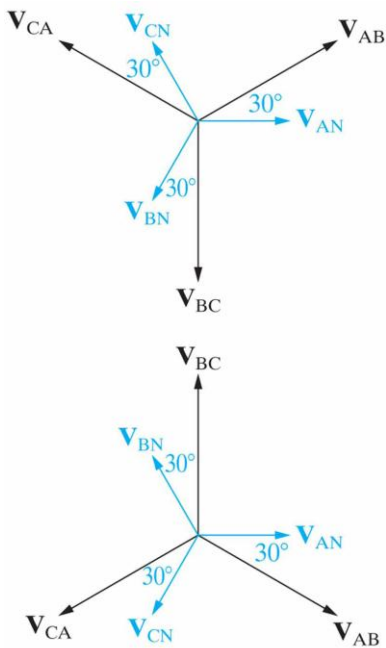
$$\vec{I}_{aA} = (\sqrt{3}\angle -30^\circ)\vec{I}_{AB} \quad \text{or} \quad I_L = \sqrt{3}I_\phi \quad [\text{magnitude only}]$$

Three-phase complex power:  $S_{3\Phi} = \sqrt{3}V_L I_L \angle \theta = P_{3\Phi} + jQ_{3\Phi}$

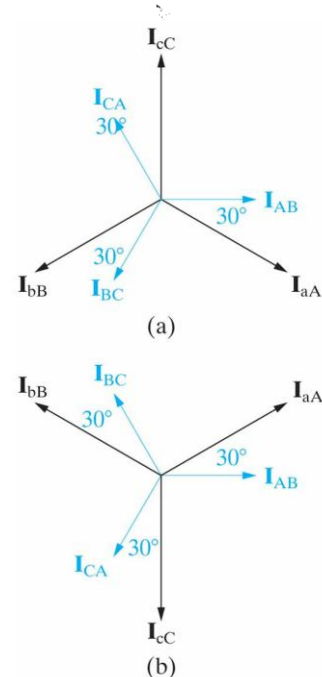
$V_L$  = line voltage magnitude

$I_L$  = line current magnitude

$\theta = \angle S = \angle Z = \angle \vec{V} - \angle \vec{I} = \text{power factor angle}$



Phasor diagrams showing the relationship between line-to-line and line-to-neutral voltages in a balanced system. (a) The abc sequence. (b) The acb sequence



Phasor diagrams showing the relationship between line currents and phase currents in a Δ-connected load. (a) The positive sequence. (b) The negative sequence.